SEISMIC MONITORING OF CARBON DIOXIDE FLUID FLOW

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Introduction. I

- Storage of CO₂ in geological formations is a procedure employed to reduce the amount of greenhouse gases in the atmosphere to slow down global warming.
- Geologic sequestration involves injecting CO₂ into a target geologic formation at depths typically >1000 m where pressure and temperature are above the critical point for CO₂ (31.6C, 7.38 MPa).
- First industrial scale CO₂ injection project: Sleipner gas field (North Sea).

Introduction. II

- CO₂ is separated from natural gas produced and is currently being injected into the Utsira Sand, a saline aquifer at the Sleipner field, some 26000 km² in area.
- Injection started in 1996 and is planned to continue for about 20 years, at a rate of about one million tonnes per year.
- Time-lapse seismic surveys aim to monitor the migration and dispersal of the CO₂ plume after injection.
- Very little is known about the effectiveness of CO₂ sequestration over very long periods of time.

Introduction. III

- The analysis of CO₂ underground storage safety in the long term is a current area of research.
- We present a methodology integrating numerical simulation of CO₂-brine flow and seismic wave propagation to model and monitor CO₂ injection.
- The model of the formation is based on the porosity and clay content distribution considering the variation of properties at the site with fluid pressure and saturation.

Presentation Outline

- Present the two-phase fluid flow equations used to simulate CO₂ injection.
- Describe a viscoelastic model for wave propagation
- Present a petrophysical model of a shaly sandstone
 based on fractal porosity and clay content, considering
 the variation of properties with pressure and saturation.
- Show numerical simulations of CO₂ injection and time-lapse seismics to monitor the migration and dispersal of CO₂ after injection in the Utsira formation at the Sleipner field in the North Sea.

The Black-Oil formulation

- The simultaneous flow of brine and CO₂ is described by the well-known Black-Oil formulation applied to two-phase, two component fluid flow.
- In the Black-Oil model employed, brine is NOT present, OIL is identified with brine and CO₂ is identified with GAS.
- Also, CO₂ may dissolve in brine (OIL) but brine (OIL) is not allowed to vaporize into the CO₂ phase.
- This formulation uses, as a simplified thermodynamic model, the quantities R_s, B_b and B_{CO2} as PVT data:

The Black-Oil formulation of two-phase flow in porous media. I

 R_s = ^{V_{dCO2}}/_{V_b^{SC}}: CO₂ solubility in brine

 B_{CO2} = ^{V_{CO2}}/_{V_{CO2}^{SC}}: CO₂ formation volume factor

 B_b = ^(V_{dCO2}^{res} + V_b^{res})/_{V_b^{SC}}: brine formation volume factor

To estimate the above PVT data we used an algorithm developed by Hassanzadeh (2008).

The Black-Oil equations for two-phase flow in porous media are obtained combining conservation of mass of each component with two-phase Darcy's law.

The Black-Oil formulation of two-phase flow in porous media. II

$$\nabla \cdot \left[\frac{\underline{\kappa}k_{rCO2}}{B_{CO2}\eta_{CO2}} (\nabla p_{CO2} - \rho_{CO2}g\nabla D) + \frac{\underline{\kappa}R_sk_{rb}}{B_b\eta_b} (\nabla p_b - \rho_bg\nabla D) \right]$$
$$+ q_{CO2} = \frac{\partial \left[\phi \left(\frac{S_{CO2}}{B_{CO2}} + \frac{R_sS_b}{B_b} \right) \right]}{\partial t}$$

$$\nabla \cdot \left[\frac{\underline{\kappa}k_{rb}}{B_b\eta_b}(\nabla p_b - \rho_b g \nabla D\right] + q_b = \frac{\partial \left[\phi \frac{S_b}{B_b}\right]}{\partial t}$$

Two algebraic equations complete the system:

$$S_b + S_{CO2} = 1$$
, $p_{CO2} - p_b = P_C(S_b)$

Numerical solution of the Black-Oil formulation of twophase flow in porous media.

The unknowns for the Black-Oil fluid-flow model are the fluid pressures p_{CO2} , p_b and the saturations S_{CO2} , S_b for the CO₂ and brine phases.

They were computed using the public domain software **BOAST**, which solves the differential equations applying **IMPES**, a finite difference technique.

Seismic modeling. Mesoscopic attenuation effects. I

- An important mechanisms of P-wave attenuation and dispersion at seismic frequencies is known as mesoscopic loss, due to heterogeneities larger than the pore size but much smaller than the predominant wavelengths (mesoscopic-scale heterogeneities).
- These effects are due to the equilibration of wave-induced fluid pressure gradients via a slow-wave diffusion process (Type II Biot waves).
- White et al. (1975) were the first to introduce the mesoscopic-loss mechanism in the framework of Biot's theory, which is illustrated in the next figures.

Traces of waves travelling through a porous media saturated by gas (top left), water

(top right) and periodic gas-water (bottom)



-1e-05

-2e-05

100

200

time (ms)

300

SEISMIC MONITORING OF CARBON DIOXIDE FLUID FLOW - p. 11

400

Traces of waves for the gas, water and periodic gas-water saturation cases



The delay in the arrival time in the periodic case is due to the velocity dispersion caused by the mesoscopic scale heterogeneities. Attenuation and dispersion in the periodic gas-water case is in perfect agreement with that predicted by White's theory. SEISMIC MONITORING OF CARBON DIOXIDE FLUID FLOW - p. 12

Representative sample for 10% fluid mixture CO₂ patchy saturation.



Side length 50 cm, fractal dimension D=2.5, correlation length a = 5cm. Black zones: pure CO₂ saturation, white zones: pure brine saturation.

Computed Vp (P-wave phase velocity) as function of CO₂ patchy saturation



CO₂ is in gaseous state, fractal dimension D=2.5, correlation length a = 5 cm

Computed inverse quality factor as function of fluid mixture CO₂ patchy saturation



CO₂ is in gaseous state, fractal dimension D=2.5, correlation length a = 5 cm

SEISMIC MONITORING OF CARBON DIOXIDE FLUID FLOW - p. 15

Seismic modeling. Mesoscopic attenuation effects. II

- Due to the extremely fine meshes needed to properly represent these type of media, numerical simulations at the macroscale is very expensive or even not feasible.
- Our approach: employ an upscaling procedure to include the mesoscale effects in the macroscale.

Seismic modeling. Mesoscopic attenuation effects. III

Within the Utsira formation, determine complex and frequency dependent P-wave modulus

 $E(\omega) = \lambda(\omega) + 2\mu(\omega)$

- at the mesoscale using White's theory for patchy saturation.
- $\lambda(\omega), \mu(\omega)$: Lamé coefficients
- ω : angular frequency

Seismic modeling. Mesoscopic attenuation effects. IV

Shear wave attenuation is taken into account using another relaxation mechanism related to the P-wave White mechanism to make the shear modulus

 $\mu(\omega)$

complex and frequency dependent.

These complex moduli define an equivalent viscoelastic model at the macroscale that take into account dispersion and attenuation effects occuring at the mesoscale.

Seismic modeling.

Outside the Utsira formation and zones where only brine is present, the complex bulk and shear moduli as function of frequency were determined using a Zener model.

The dimensionless complex modulus of a Zener element is

$$Z(\omega) = \frac{\tau_{\sigma}}{\tau_{\epsilon}} \left[\frac{1 + i\omega\tau_{\epsilon}}{1 + i\omega\tau_{\sigma}} \right]$$

 $\tau_{\epsilon}, \tau_{\sigma}$: relaxation times.

The Zener model

The associated quality factor is

$$Q(\omega) = \frac{\operatorname{Re}(Z(\omega))}{\operatorname{Im}(Z(\omega))}$$

Its minimum value is equal to

$$Q_0 = \frac{2x}{x^2 - 1}, \qquad x = \left(\frac{\tau_{\epsilon}}{\tau_{\sigma}}\right)^{1/2}$$

(1)

and is located at $\omega_0 = \frac{1}{(\tau_\sigma \tau_\epsilon)^{1/2}}$. If ω_0 and Q_0 are chosen as data, then

$$\tau_{\epsilon} = \frac{x}{\omega_0}, \qquad \tau_{\sigma} = \frac{x^{-1}}{\omega_0}, \quad \text{where } x \text{ solves}(1)$$

Seismic modeling. Constitutive Relations

 $u = u(\omega) = (u_x(\omega), u_z(\omega))$: Time-Fourier transform of the displacement vector Stress-strain relations in the space-frequency domain:

$$\sigma_{jk}(u) = \lambda(\omega) \nabla \cdot u \delta_{jk} + 2\mu(\omega) \varepsilon_{jk}(u),$$

 $\sigma_{jk}(u)$: stress tensor $\varepsilon_{jk}(u)$: strain tensor δ_{jk} : Kroenecker delta

 $\lambda(\omega), \mu(\omega)$: complex Lamé coefficients determined using White's theory.

Seismic modeling. Phase velocities and attenuation coefficient.

For isotropic viscoelastic solids, the frequency dependent phase velocities $v_t(\omega)$ and quality factors $Q_t(\omega)$, t = p, s are defined by the relations

$$v_t(\omega) = \left[\operatorname{Re}\left(\frac{1}{vc_t(\omega)}\right) \right]^{-1}, Q_t(\omega) = \frac{\operatorname{Re}(vc_t(\omega)^2)}{\operatorname{Im}(vc_t(\omega)^2)}, t = p, s$$

 $vc_p(\omega), vc_s$: complex and frequency dependent compressional and shear velocities defined as

$$vc_p(\omega) = \sqrt{\frac{E(\omega)}{\rho}}, \quad vc_s(\omega) = \sqrt{\frac{\mu(\omega)}{\rho}}$$

ρ : bulk density.

Seismic modeling. A viscoelastic model for wave propagation. I

Equation of motion in a 2D isotropic viscoelastic domain Ω with boundary $\partial \Omega$:

$$\omega^2 \rho u + \nabla \cdot \sigma(u) = f(x, \omega), \quad \Omega$$

First-order absorbing boundary condition:

$$-\sigma(u)\nu=i\omega\mathcal{D}u,\quad\partial\Omega,$$

 $f(x, \omega)$ external source

Numerical Solution - Finite Element Method.

- The FE was computed at a selected number of frequencies in the range of interest using an iterative finite element domain decomposition procedure.
- The time domain solution was obtained using a discrete inverse Fourier transform.
- To approximate each component of the solid displacement vector we employed a nonconforming finite element space which generates less numerical dispersion than the standard bilinear elements.
- The error measured in the energy norm is of order $h^{1/2}$, where *h* is the size of the computational mesh. SEISMIC MONITORING OF CARBON DIOXIDE FLUID FLOW – p. 24

A petrophysical model of the Utsira formation.

We consider a 2D model of the Utsira formation constructed using an initial porosity ϕ_0 (at hydrostatic pore pressure) and the clay content *C* of the formation.

The model was constructed using iteratively a wave propagation simulator to fit the avalaible seismic data. It has 400 m thickness (top at 800 m and bottom 1200 m b.s.l.).

Within the formation, there are several mudstone layers which act as barriers to the vertical motion of the CO₂.

A petrophysical model considering pressure and saturation variations. I

Our shaly sand model was generated using fractal realizations of the porosity ϕ_0 at hydrostatic pressure p_H and clay content *C*.

To determine the porosity ϕ as function of the fluid pressure p_f (obtained from the flow simulator) we solved the nonlinear equation:

$$\frac{(1-\phi_c)}{K_s}(p_f - p_H) = \phi_0 - \phi + \phi_c \ln \frac{\phi}{\phi_0},$$

$$\phi_c : \text{critical porosity}$$

A petrophysical model considering pressure and saturation variations. II

The bulk modulus of the dry matrix was determined using a Krief model (A = 4.5):

$$K_m = K_s (1-\phi)^{A/(1-\phi)}.$$

Here *K_s* denote the bulk modulus of the solid grains.

Assuming a Poisson medium the shear modulus of the solid grains is $\mu_s = 3K_s/5$ and the following relation gives the shear modulus of the dry matrix

$$\mu_m = \mu_s (1-\phi)^{A/(1-\phi)}.$$

A petrophysical model considering pressure and saturation variations. III

Horizontal κ_x and vertical permeability κ_z ,

$$\frac{1}{\kappa_x} = \frac{45(1-\phi)^2}{\phi^3} \left(\frac{(1-C)^2}{R_q^2} + \frac{C^2}{R_c^2}\right)$$

R_q, *R_c*: average radii of sand and clay particles

$$\frac{\kappa_x}{\kappa_z} = \frac{1 - (1 - 0.3a)\sin\pi S_b}{a(1 - 0.5\sin\pi S_b)}$$

a: permeability-anisotropy parameter

Porosity map of the formation.



Permeability map (Darcy units) of the formation.



CO₂ Injection model. I

- At the Utsira formation CO₂ is injected at a constant flow rate of one millon tons per year.
- The injection point is located at the bottom of the Utsira formation: x = 600 m, z = 1060 m.
- The viscosity, density and bulk modulus of CO₂ needed for the flow simulator were obtained from the Peng-Robinson equations as a function of temperature and pore pressure.

Injection Modeling. II



CO₂ saturation distribution after 2 years (left) and 6 years(right) of CO₂ injection

SEISMIC MONITORING OF CARBON DIOXIDE FLUID FLOW - p. 32

Seismic Model.

- The equivalent viscoelastic model, determined using White's model for patchy saturation, assumes an effective single-phase fluid.
- Effective fluid density, viscosity and bulk modulus were obtained using the properties of the CO₂ and brine weighted by the corresponding saturations computed by the BOAST flow simulator.
- The next Figure displays maps of of P-wave phase velocity v_p(ω) and attenuation coefficient Q_p(ω) at 50 Hz after 2 years of CO₂ injection.

P-wave phase velocity $v_p(\omega)$ (m/s) (left) and attenuation coefficient $Q_p(\omega)$ (right) at 50

Hz.



Observe a decrease in P- wave velocity in zones of CO₂ accumulation (left) and a

corresponding decrease in attenuation coefficient Q_p (right). SEISMIC MONITORING OF CARBON DIOXIDE FLUID FLOW – p. 34

S-wave phase velocity $v_s(\omega)$ (m/s) (left) and attenuation coefficient $Q_s(\omega)$ (right) at 50

Hz.



Observe a decrease in S- wave velocity in zones of CO₂ accumulation (left) and a

corresponding decrease in attenuation coefficient Q_s (right). SEISMIC MONITORING OF CARBON DIOXIDE FLUID FLOW – p. 35

Seismic Monitoring.

- To analyze the capability of seismic monitoring to identify zones of CO₂ accumulation, the model was excited with compressional point and line sources located at the top of the model (800 m depth) with central frequency 50 Hz.
- The viscoelastic wave equation was solved for 200 frequencies. The time domain solution was obtained using an inverse Fourier transform.
- The next Figures display snapshots at several steps of the simulations. Other Figures show time histories before and after 2 and 6 years of CO₂ injection.

Snapshots of z-component of particle velocity at 100 ms (left) and 150 ms (right). Point

Source.



Snapshots of z-component of particle velocity at 180 ms (left) and 200 ms (right). Point

Source.



Snapshots of z-component of particle velocity at 220 ms (left) and 280 ms (right). Point

Source.



Time histories of the z-component of the particle velocity measured at the top of the

model before and after 2 years of CO₂ injection. Point Source



Time histories before and after 2 years of CO_2 injection. Point Source. Both figures are

shown with the SAME SCALE



Traces of the z-component of the velocity before (left) and after 2 years (right) CO₂ injection. The first strong and second weak arrivals seen on the left Figure come from the base and top of the Utsira. The strong later arrivals seen on the right Figure are due to P-waves reflected at the CO₂ accumulations and the base of the Utsira. Time histories before and after 2 years of CO_2 injection. Line Source. Both figures are

shown with the SAME SCALE



Traces of the z-component of the particle velocity before (left) and after 2 years (right) CO₂ injection. The two arrivals seen on the left Figure come from the base and top of the Utsira. The strong later arrivals seen on the right Figure are due to P-waves reflected at CO₂ accumulations and the base of the Utsira.

Time histories before and after 2 and 6 years of CO₂ injection. Line Source



Traces of the z-component of the particle velocity after 2 years (left) and 6 years (right) of CO₂ injection. The earlier arrivals on the right Figure are due to waves reflected at the CO₂ accumulations below the shalow mudstone layers.

CONCLUSIONS

- The numerical examples show the effectiveness of combining multiphasic flow simulators in porous media with seismic monitoring to map the spatio-temporal distribution of CO₂ after injection.
- The wave propagation model includes attenuation and dispersion effects due to mesoscopic scale heterogeneities using White's theory.
- This methodology constitutes a valuable tool to monitor the migration and dispersal of the CO₂ plume and to analyze storage integrity, providing early warning should any leakage occurs.

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